

imaros

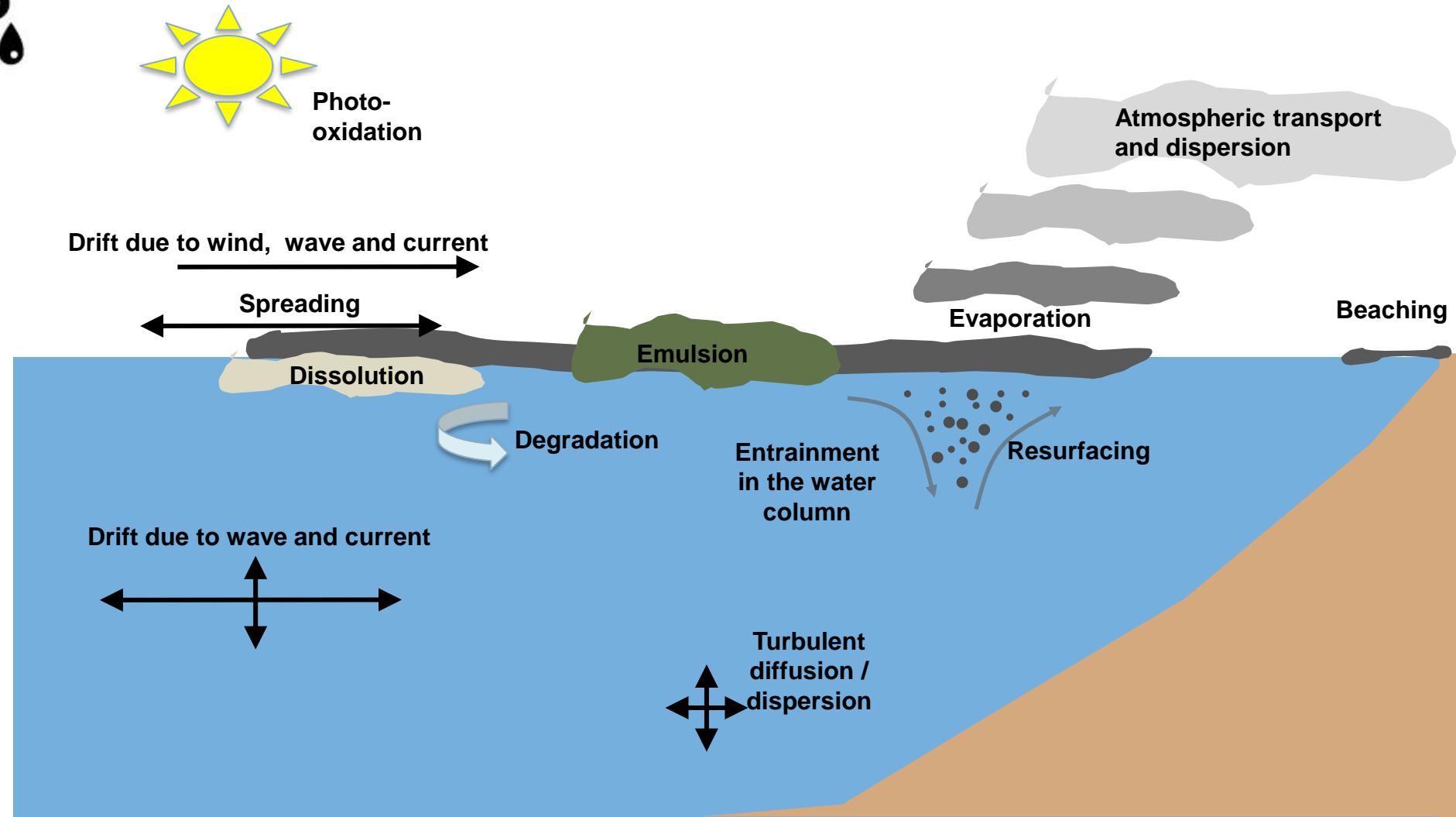


Final conference

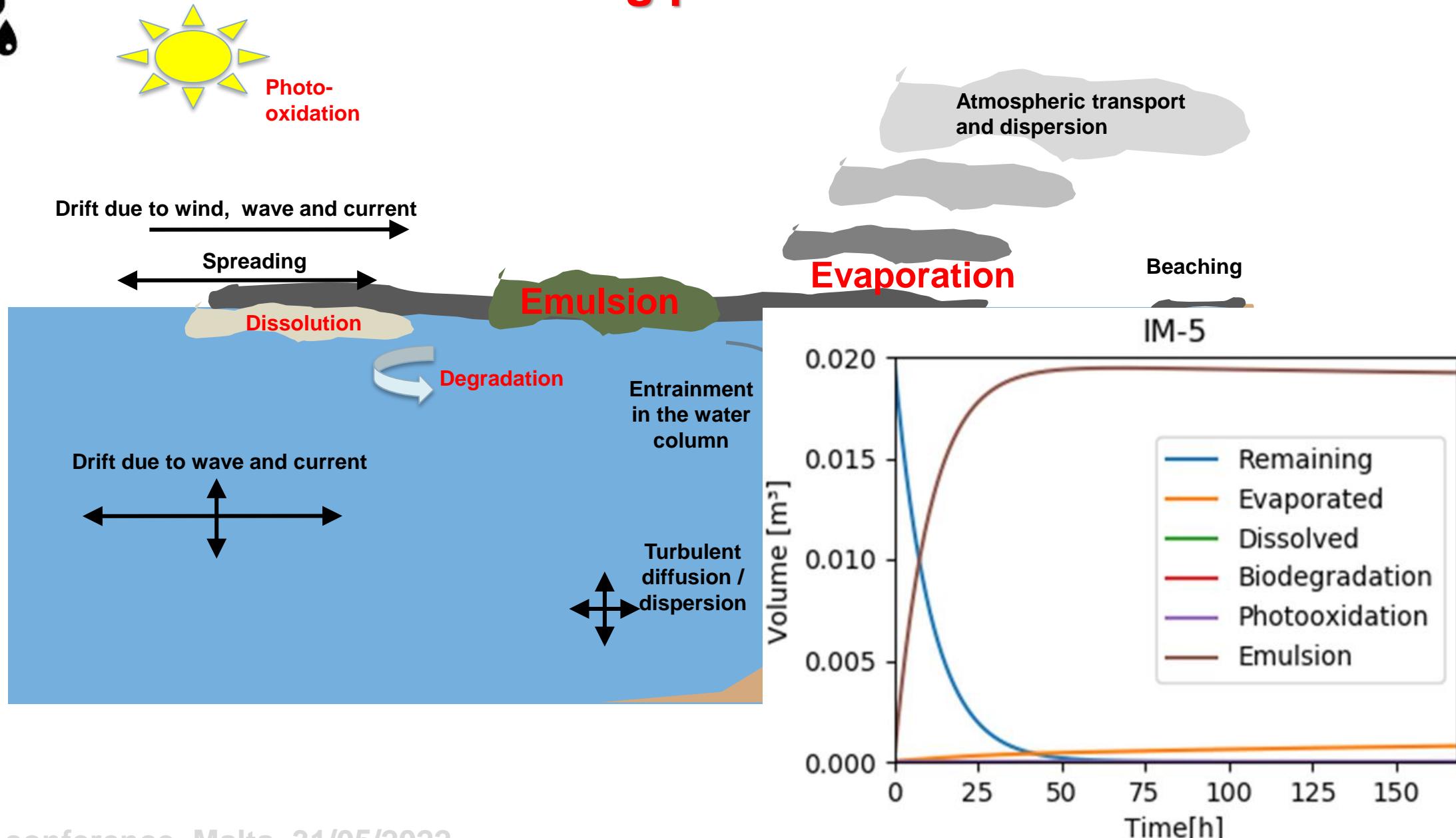
Modelling VLSFO weathering

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Oil weathering processes



Are the existing parameterizations able to simulate VLSFO weathering?

Can you trust in oil weathering
model forecast for VLSFO?

Validation/invalidation exercise

Weathering model vs polludrome data

A "toy" weathering model

Evaporation

- Lyman/Jones (as in Oiltrans)
 - Temperature
 - Wind speed
 - Slick length
 - Molar volume
 - Schmidt number in air
 - Vapor pressure
- Brighton (as in ALOHA)
 - Stability class
 - Wind speed
 - Slick length
 - Molar weight (for molecular diffusivity)
 - Vapor pressure
- Fingas (as in OSERIT)
 - 2 empirical constants

Emulsification

- Scory (as in OSERIT)
 - Wave height
 - Kem
 - C
 - Maximum water content
- Mackay
 - Wind speed
 - Maximum water content
 - C

Volatilization : Lyman

- Dissolution : Mackay and Leinonen
- Solubility
- Molar volume (for diffusion coefficient)
- Windspeed
- Water volume

Photooxidation

- Half life constant

Biodegradation

- Half life constant

Density

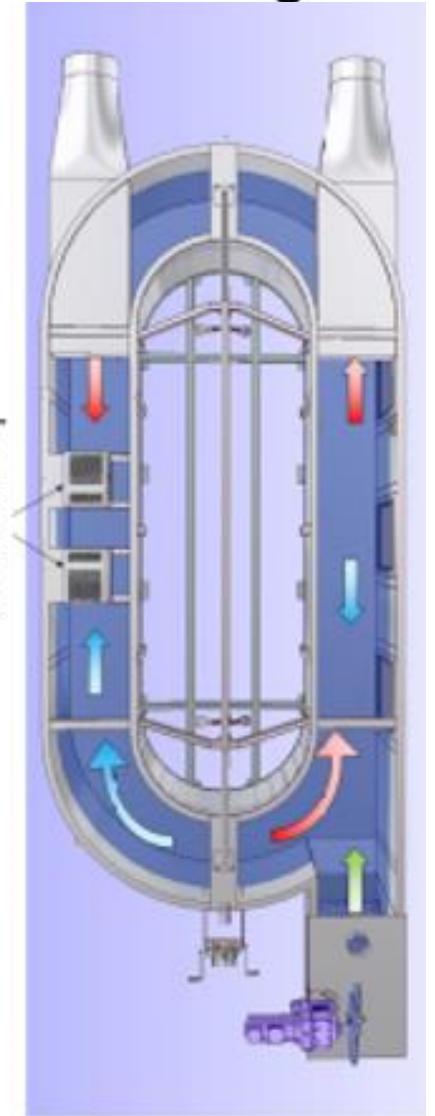
- Evap
- Dissolution
- mulsification

Viscosity : Betancour

- Temperature
- Evaporation
- Emulsion



Experimental set-up Cedre's polludrome



Polludrome geometry

- Sea water volume : 7 m³
- Sea water depth : 0,9 m
- Polludrome surface : 7.78 m²



Controlled 'environmental' conditions

- Wind : 5m/s
- Currents : 0,4m/s
- Waves height : 0,75 m
- Air temp : 15°C
- Sea water temp : 15°C



Lab characterization of benchmarked oils at 15°C

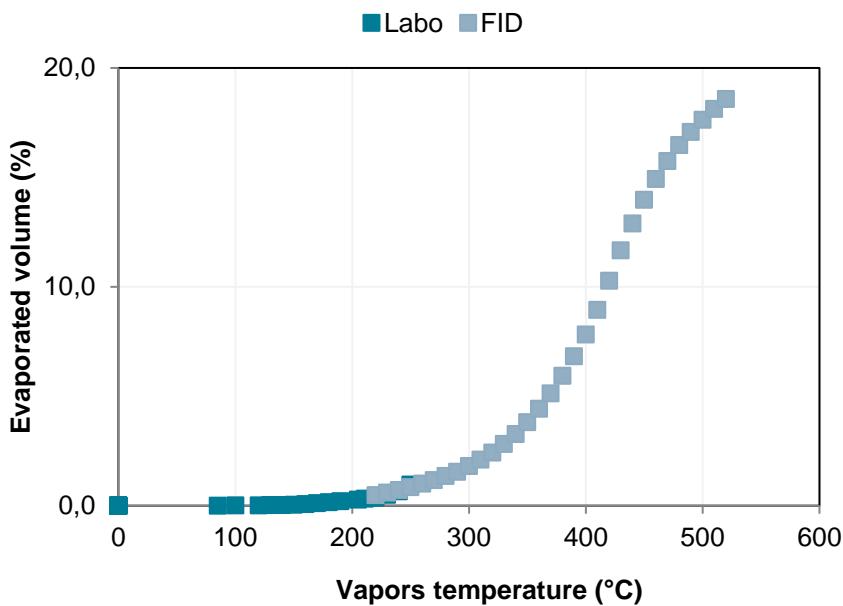
Fresh oil

At 15°C	IM-5	IM-14	IM-15
Density [kg/m ³]	909	937	951
Viscosity (10s ⁻¹) [mPa s]	3051	17121	4305
Viscosity (100s ⁻¹) [mPa s]	582*	5347	4137
Pour point [°C]	15	27*	Nd
Max water content in lab [%]	67-81	19-50	49-70
Max water content in polludrome [%]	86	57	70

* from SINTEF

Lab characterization of the oil composition

Distillation curve

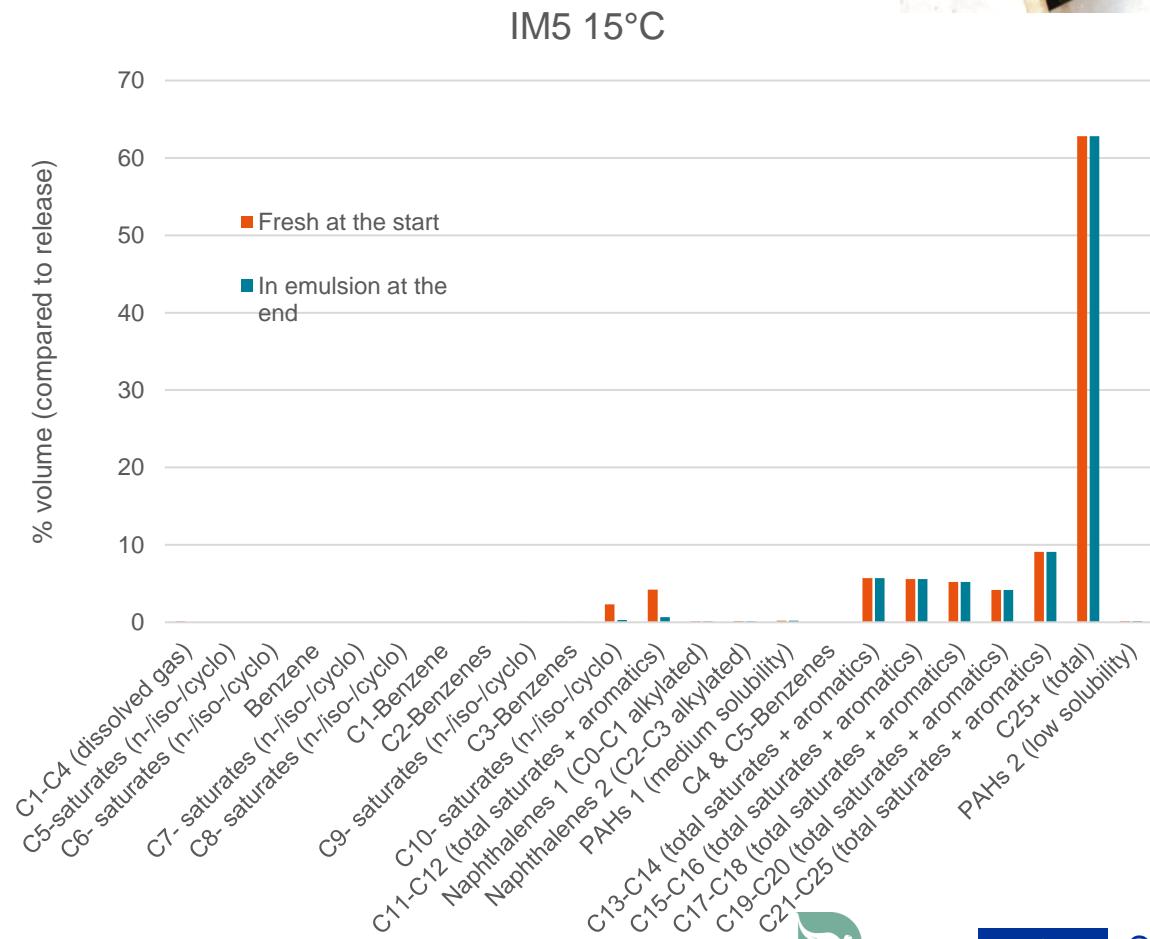
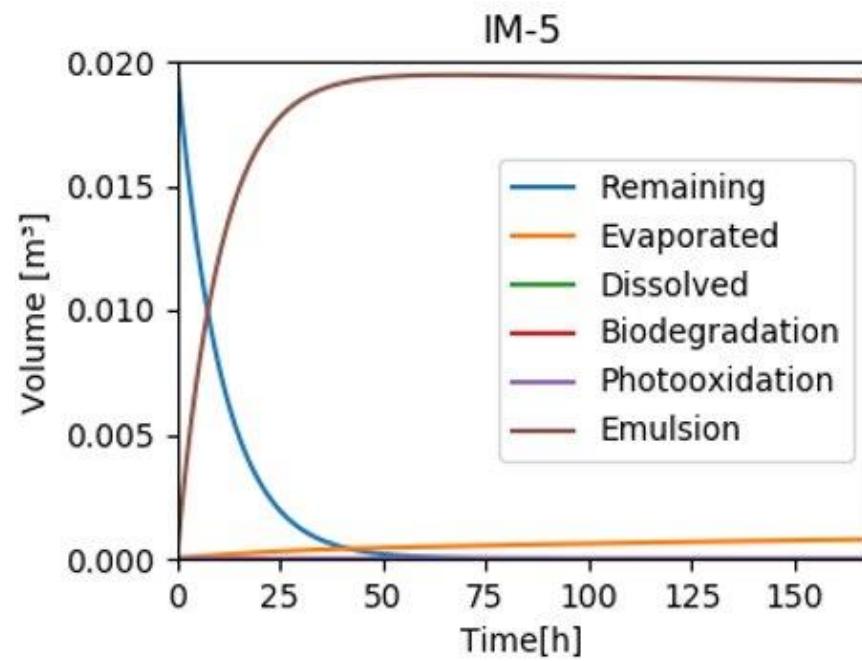


OSCAR
characterization

Individuals compounds	Composition (% weight)
C ₁ -C ₄ (dissolved gas)	0.03
C ₅ -saturates (n-/iso-/cyclo)	0.00
C ₆ - saturates (n-/iso-/cyclo)	0.00
C ₇ - saturates (n-/iso-/cyclo)	0.00
C ₈ - saturates (n-/iso-/cyclo)	0.00
C ₉ - saturates (n-/iso-/cyclo)	0.01
Benzene	0.00
C ₁ -Benzene	0.00
C ₂ -Benzenes	0.00
C ₃ -Benzenes	0.02
C ₄ & C ₅ -Benzenes	0.00
C ₁₀ - saturates (n-/iso-/cyclo)	0.00
C ₁₁ -C ₁₂ (total saturates + aromatics)	4.01
C ₁₃ -C ₁₄ (total saturates + aromatics)	4.36
C ₁₅ -C ₁₆ (total saturates + aromatics)	4.47
C ₁₇ -C ₁₈ (total saturates + aromatics)	3.29
C ₁₉ -C ₂₀ (total saturates + aromatics)	3.33
C ₂₁ -C ₂₅ (total saturates + aromatics)	5.94
C ₂₅ + (total)	71.66
Naphthalenes 1 (C ₀ -C ₁ alkylated)	0.64
Naphthalenes 2 (C ₂ -C ₃ alkylated)	0.40
PAHs 1 (medium solubility)	0.46
PAHs 2 (low solubility)	1.38
Phenols (C ₀ -C ₄)	-

Each pseudo-component is characterized by density, molar mass, molar volume, vapour pressure, boiling point, solubility, photooxidation rate, biodegradation rate,...

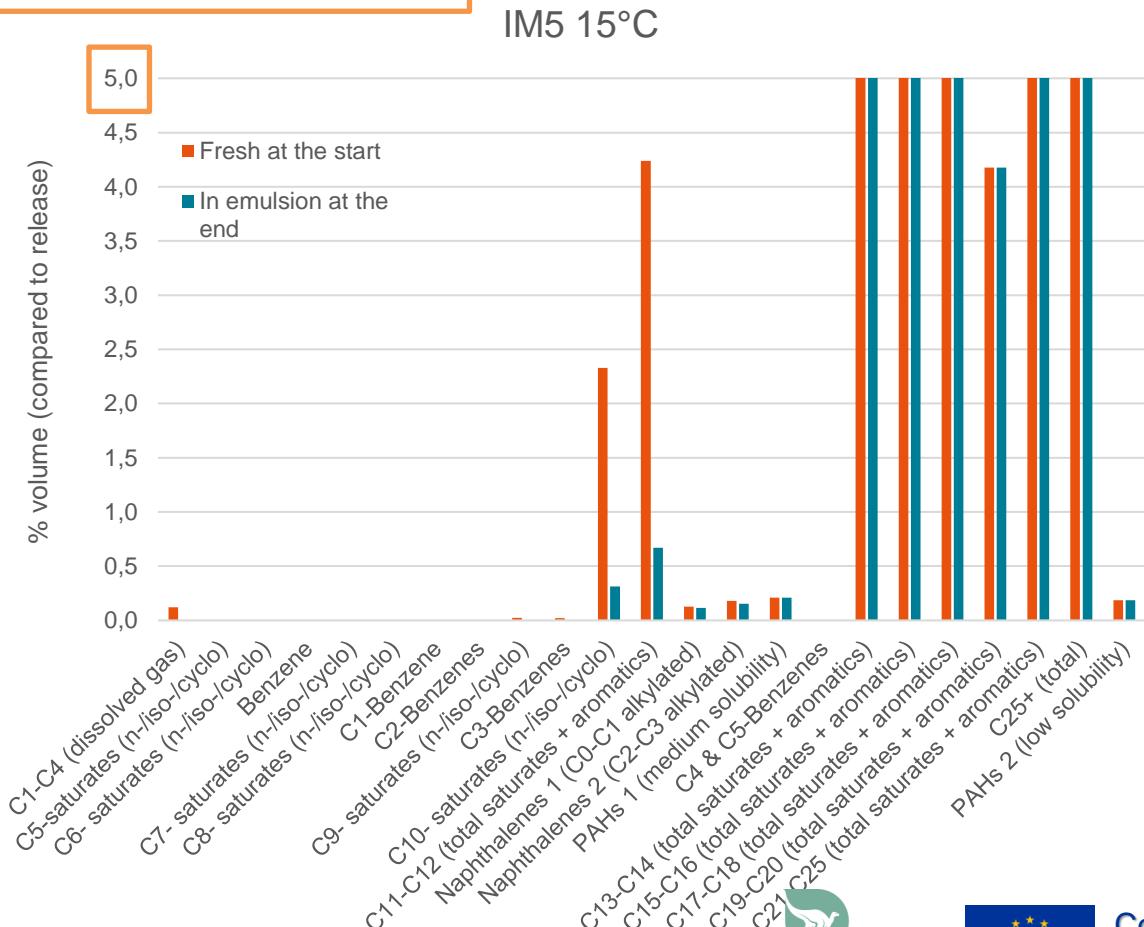
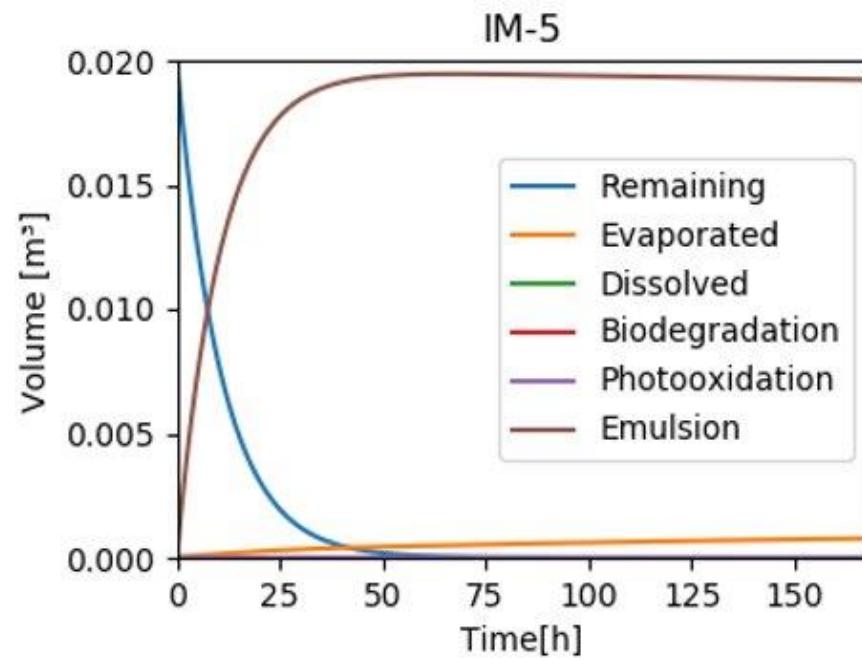
Model simulation IM-5 at 15°C



Model simulation IM-5 at 15°C



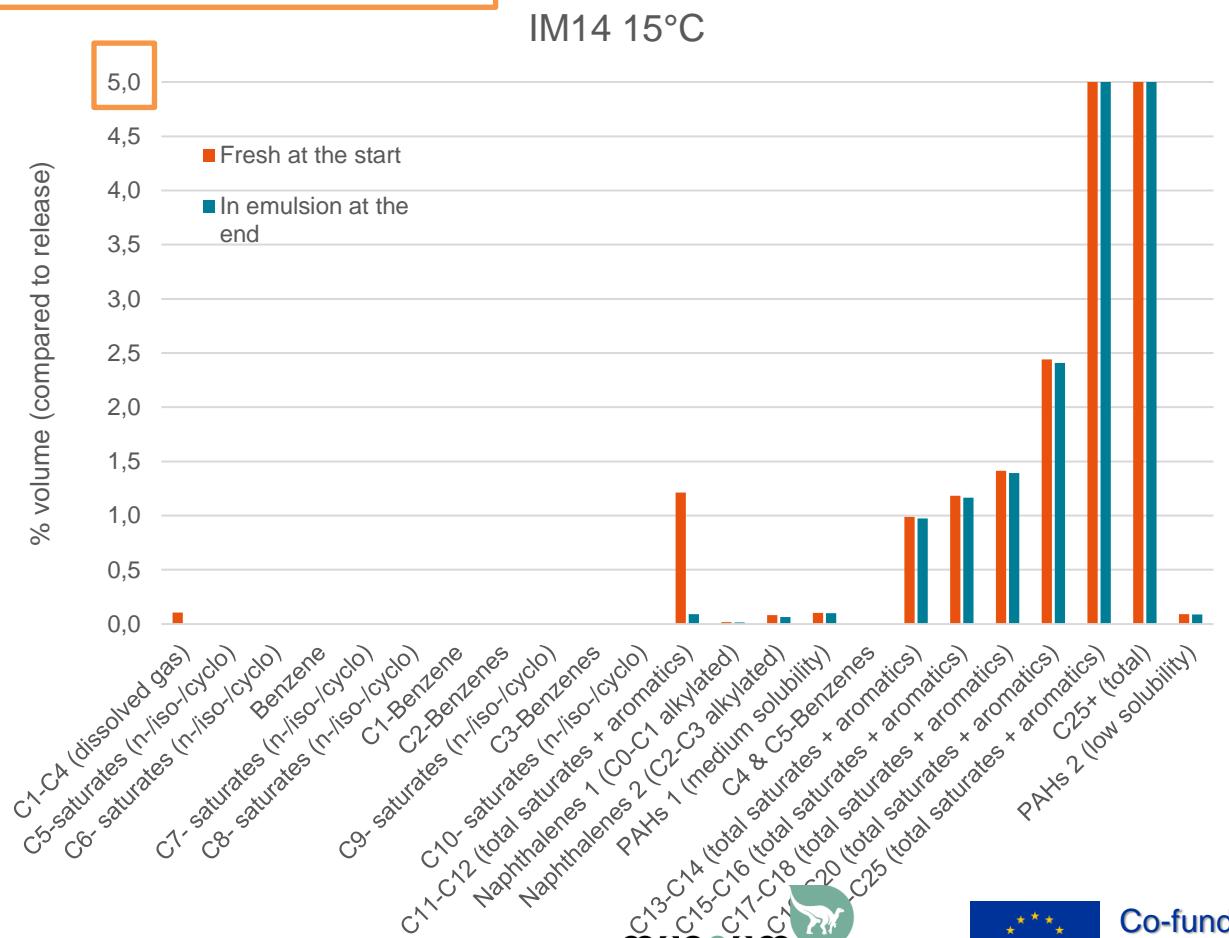
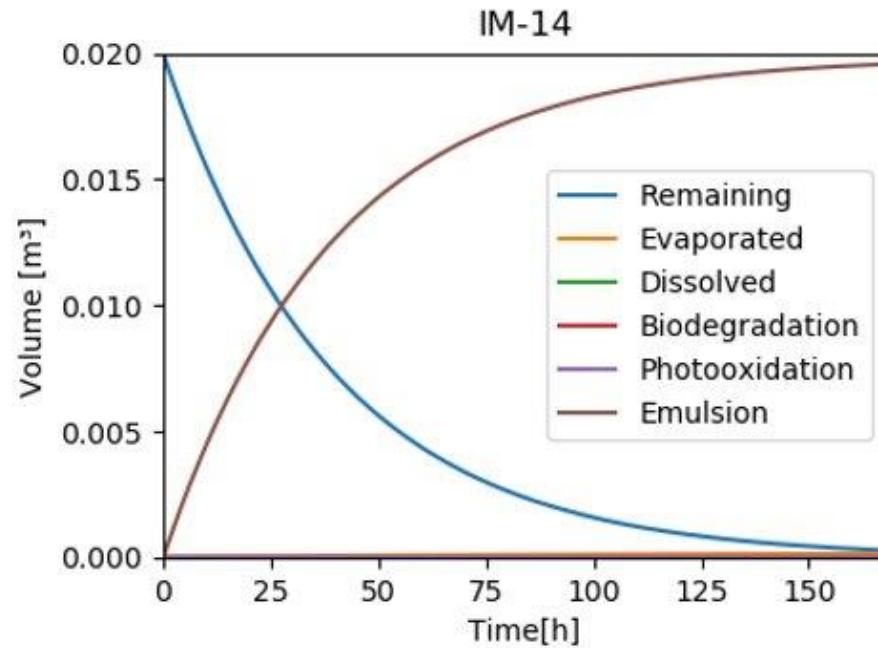
Zoom; C25+ = 62% volume



Model simulation IM-14 at 15°C



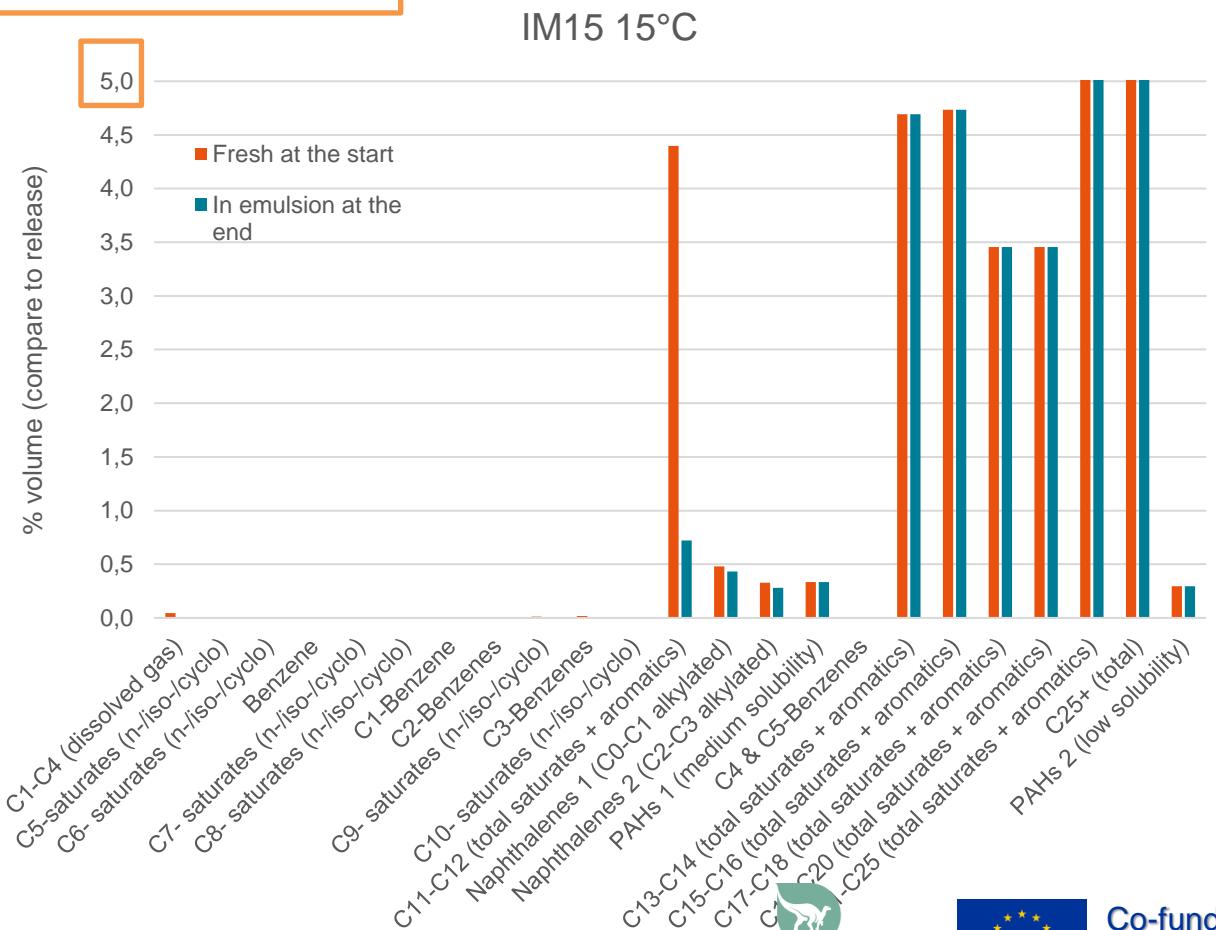
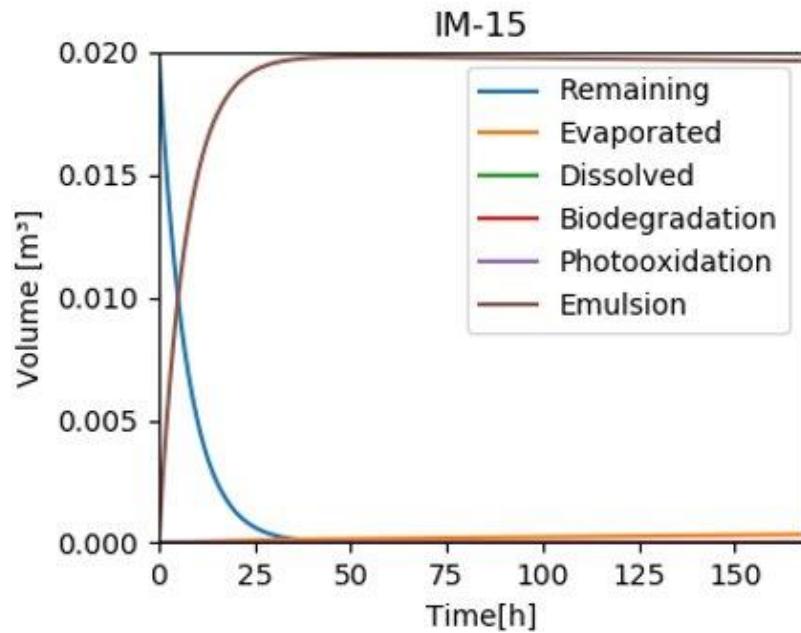
Zoom; C25+ = 81 % volume



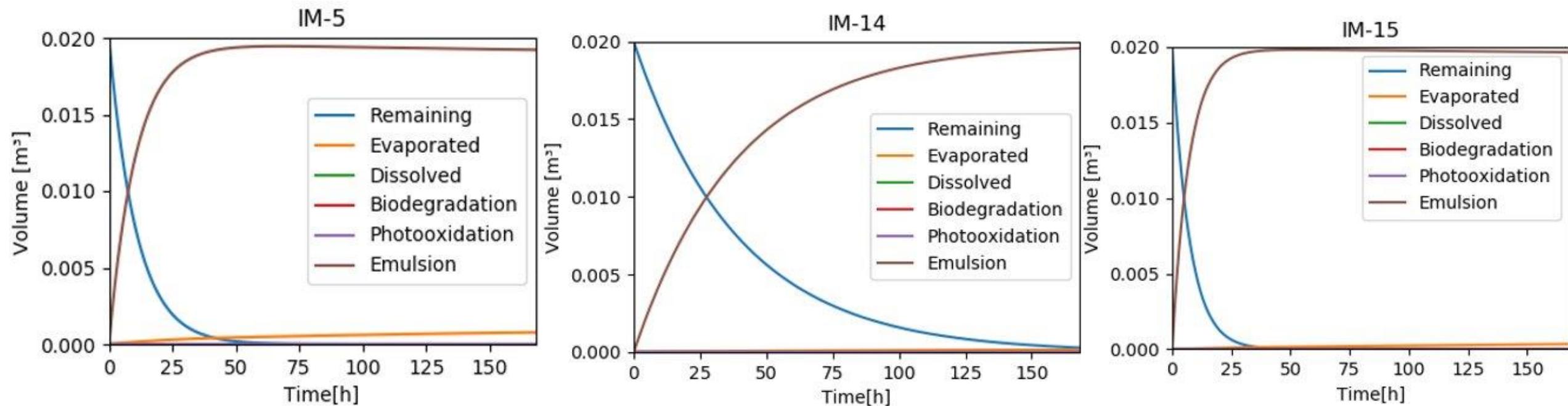


Model simulation IM-15 at 15°C

Zoom; C25+ = 71% volume

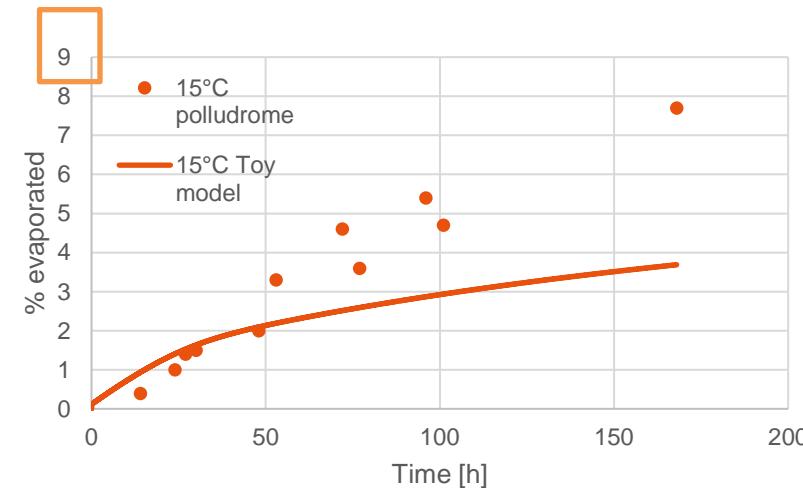


Model simulations at 15°C

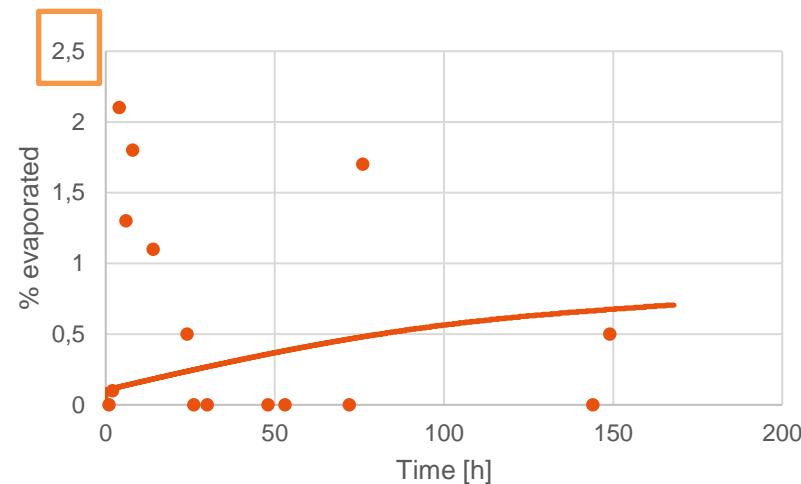


Evaporation is slightly underestimated

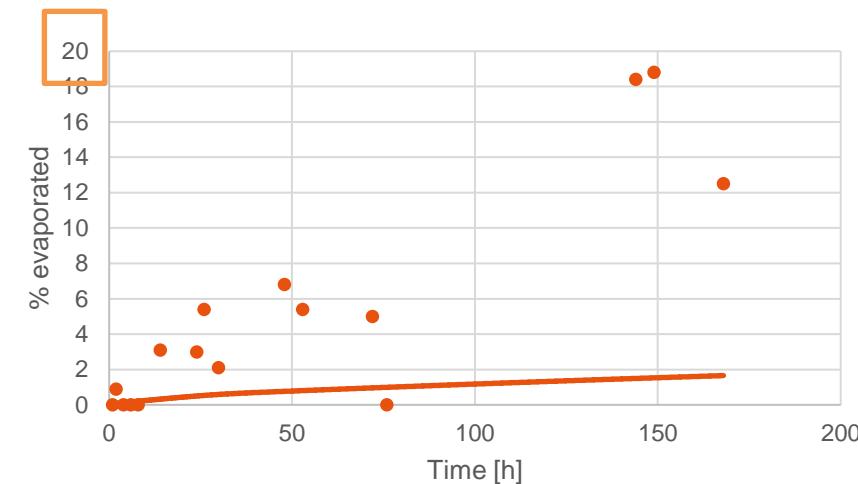
IM-5



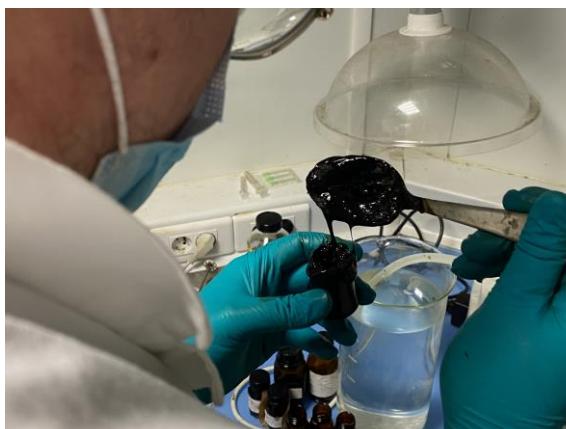
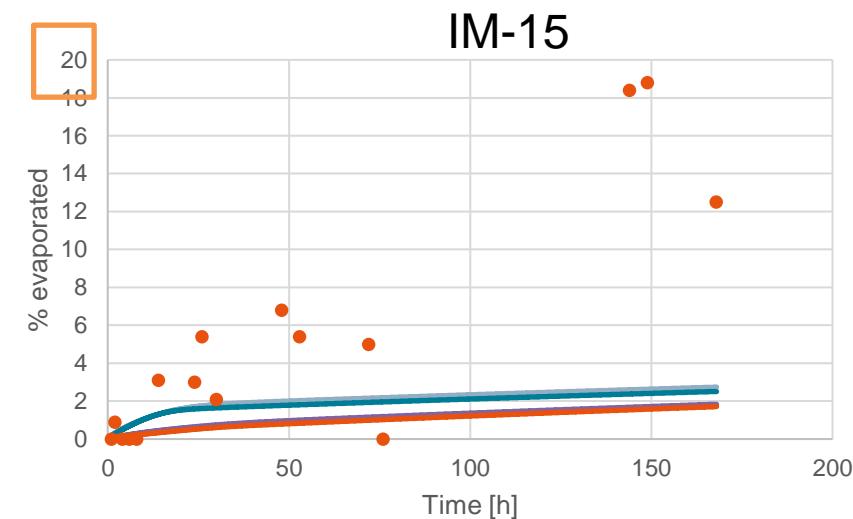
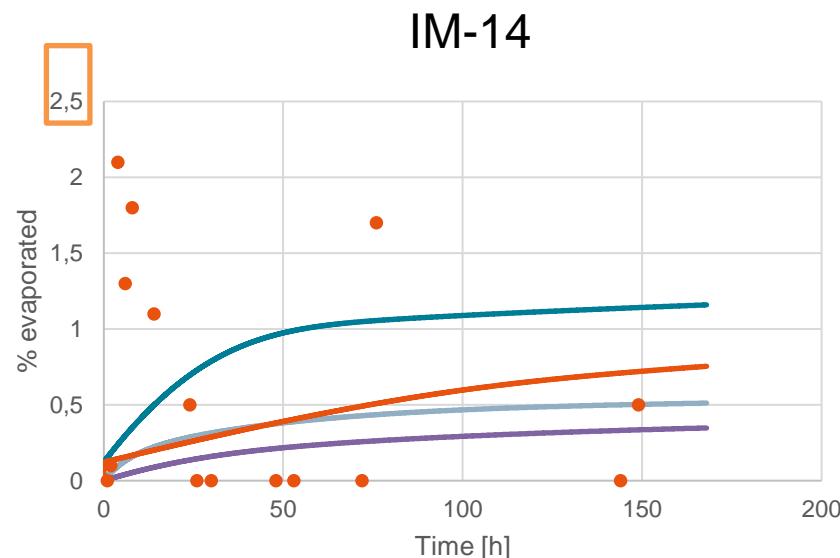
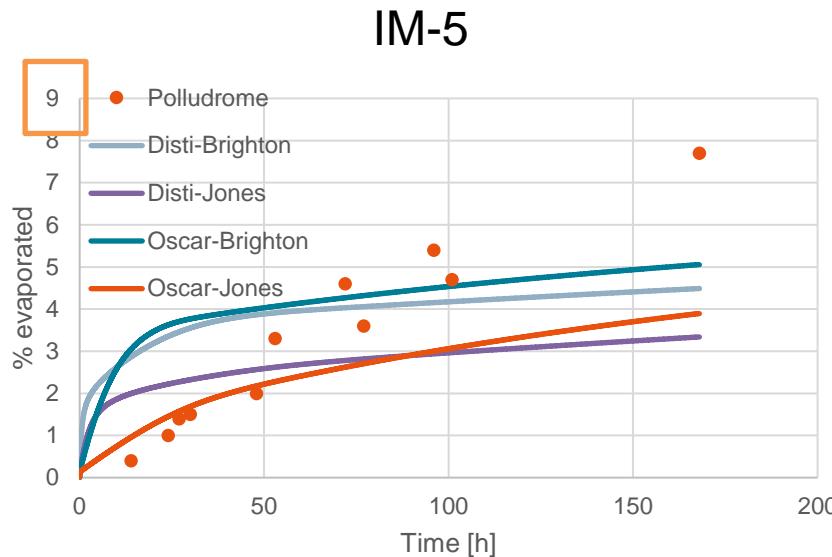
IM-14



IM-15

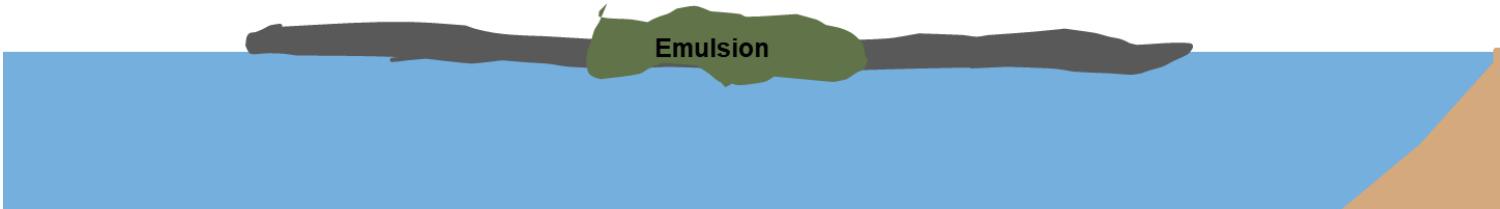


Evaporation is slightly underestimated



Emulsion

(Scory, 2005)



$$\frac{dV_{em}}{dt} = \frac{C_{18}}{1 - C_{18}} \frac{H_s}{C_{15}} V_r K_{em}$$

$$V_{water} = \frac{C_{18}}{1 - C_{18}} V_{em}$$

$$V_{tot,em} = V_{em} + V_{water} = \frac{1}{1 - C_{18}} V_{em}$$

$$V_{tot} = V_r + V_{em} + V_{water} = V_r + \frac{1}{1 - C_{18}} V_{em}$$

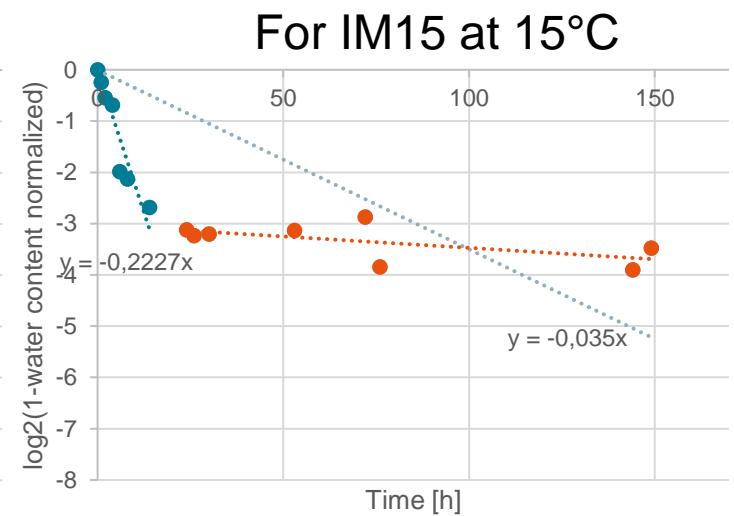
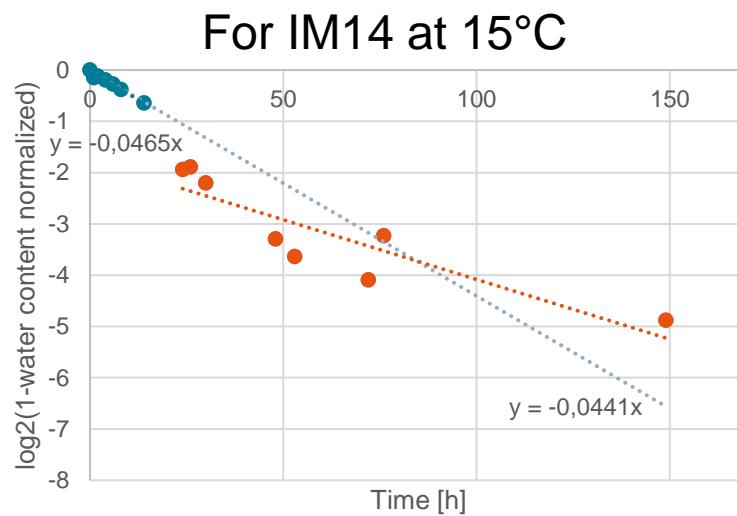
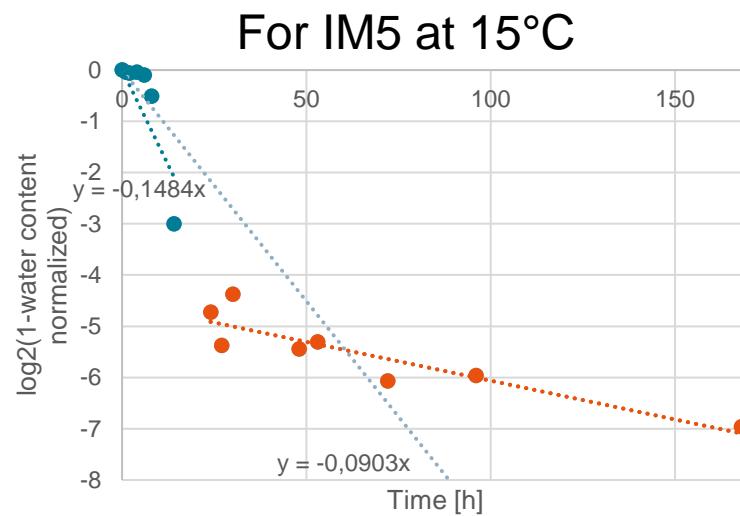
$$Y = \frac{V_{water}}{V_{tot}}$$

V_r : Volume of remaining oil [m³]
 V_{em} : Volume of emulsified oil [m³]
 V_{water} : Volume of water in the slick [m³]
 $V_{tot,em}$: Total volume of the emulsion [m³]
 V_{tot} : Total volume of the slick [m³]

Y: water fraction in the slick [%]

H_s : significant waves height [m]
 C_{15} : scaling constant (2000000 m)
 C_{18} : Maximum water content [%] (Lab)
 K_{em} : kinetic coefficient (0-120) [s⁻¹]

K_{em} can be estimated from water content evolution for the first 20h in polludrome

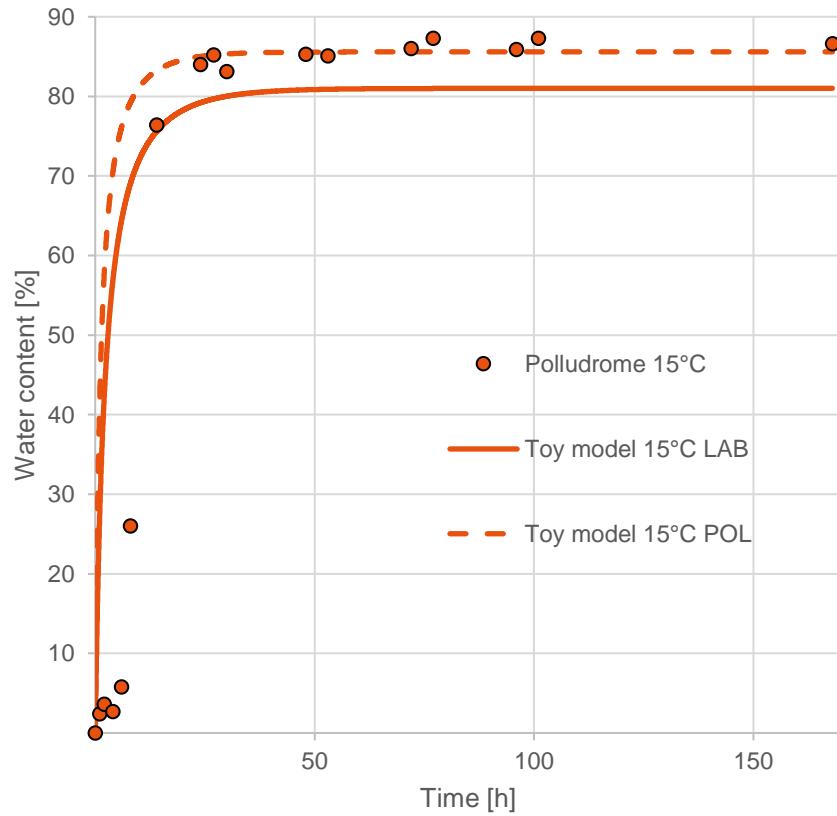


$$K_{em} = \left[t_{1/2} \frac{C_{18}}{1 - C_{18}} \frac{H_s}{C_{15}} \right]^{-1}$$

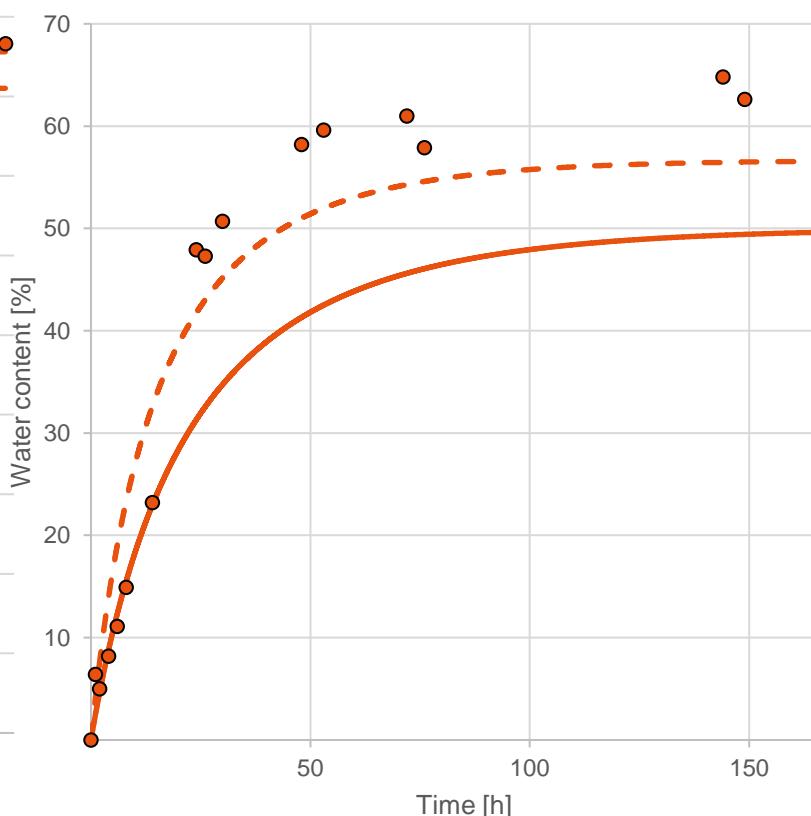
	IM-5	IM-14	IM-15
$K_{em} [\text{s}^{-1}]$	15,99	18,73	43,59

The Scory parametrization provides a good estimate of the water content [Y] uptake in the slick

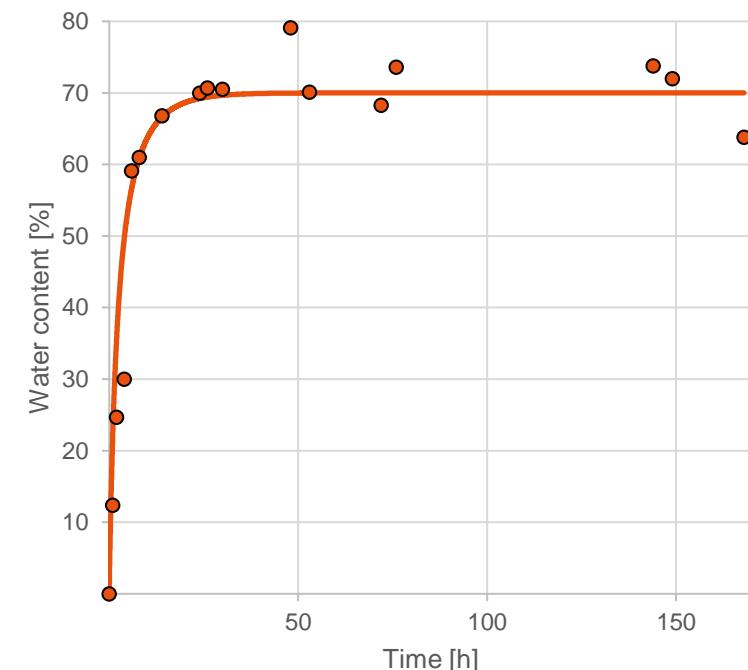
IM5



IM14



IM15

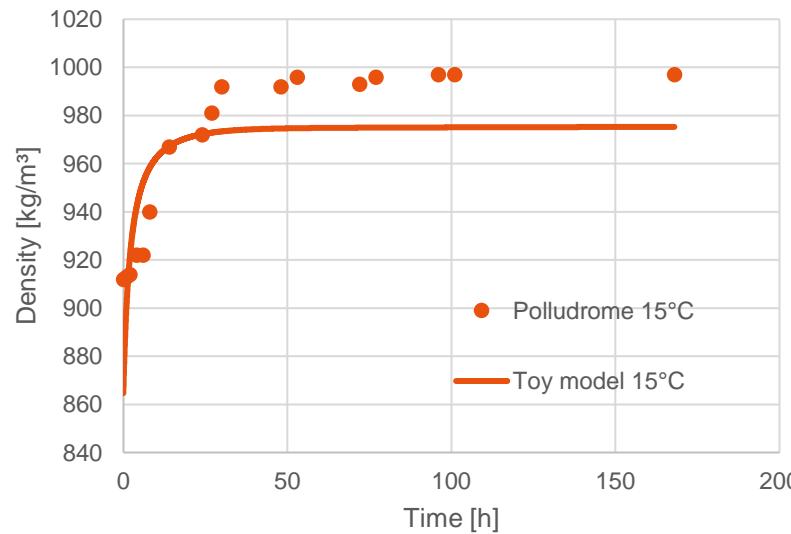


Model can simulate the evolution of the slick density if the fresh oil density is known

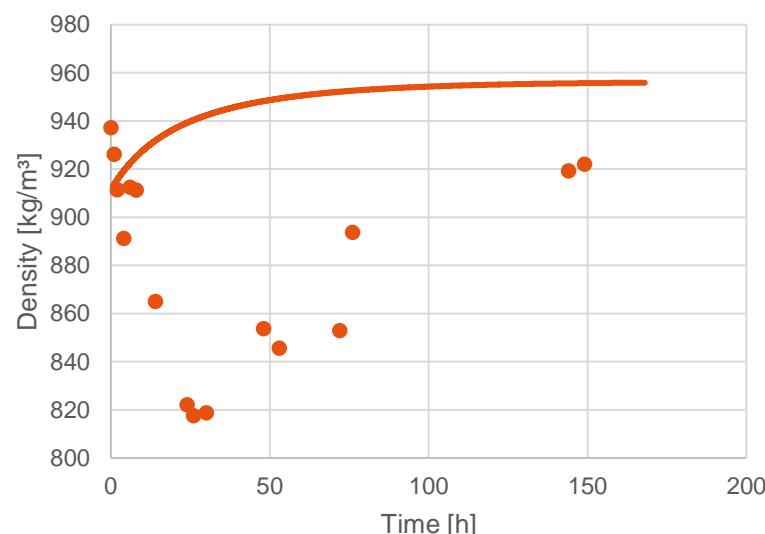
$$\rho_{C_{25+}} := \frac{\rho_{oil,fresh} V_{oil,init} - \sum \rho_i V_{i,init}}{V_{C_{25+},init}}$$

$$\rho_{slick} = \frac{\sum \rho_i V_i + \rho_{water} V_{water}}{V_{tot}}$$

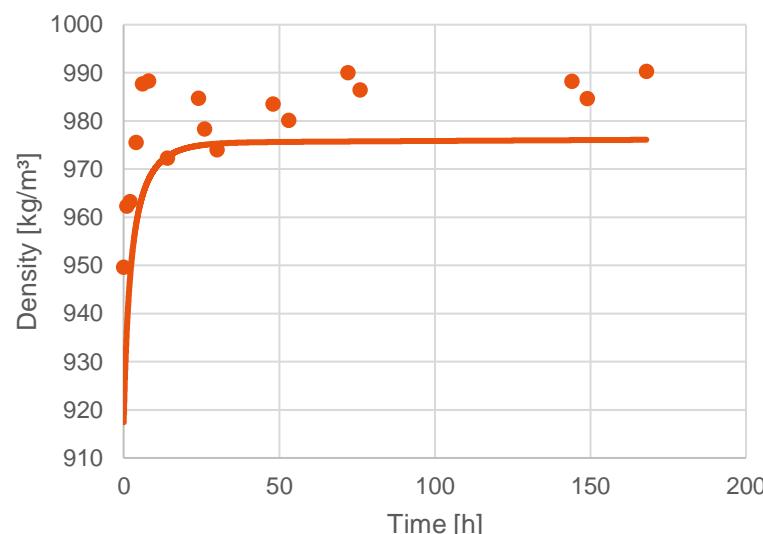
IM5



IM14



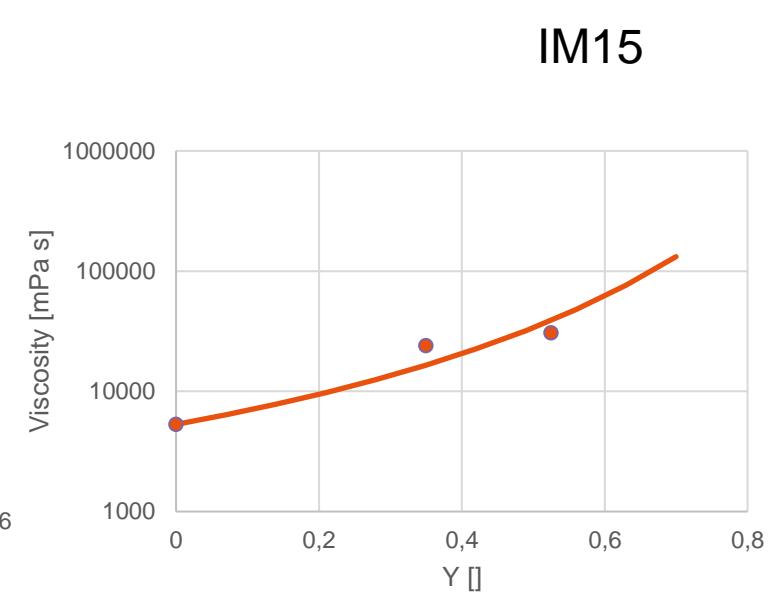
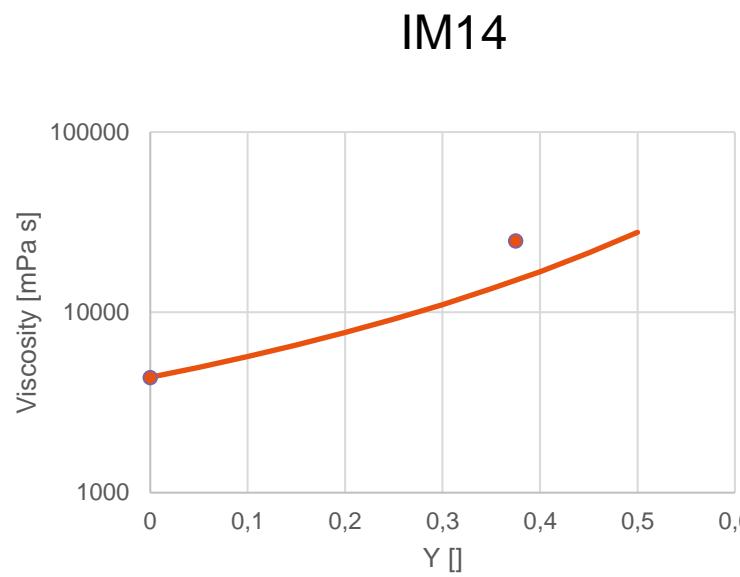
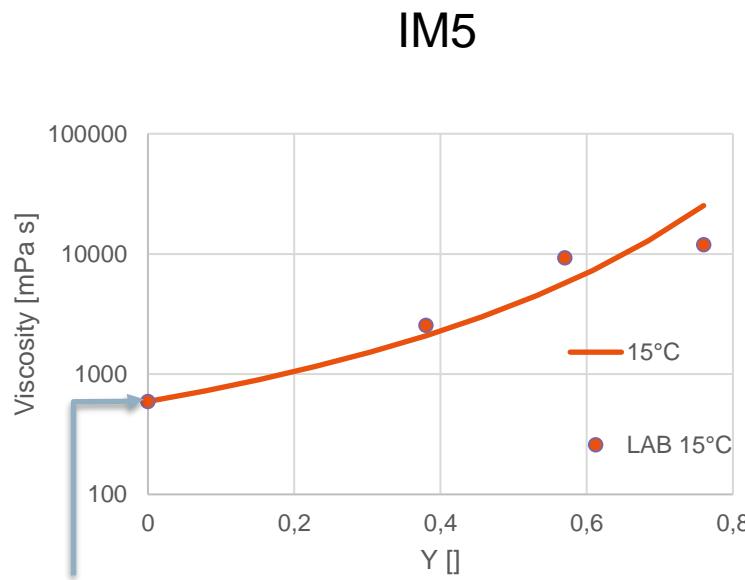
IM15



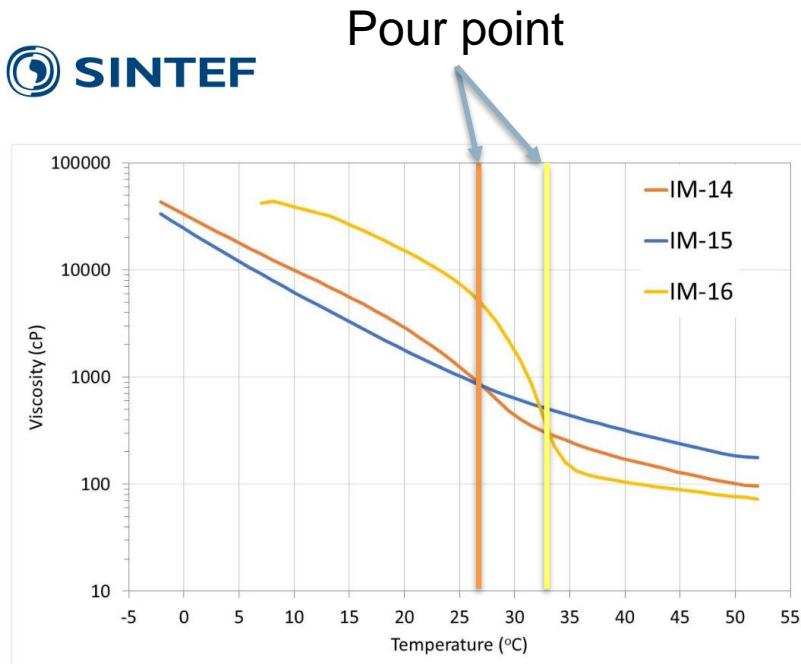
If non-emulsified oil viscosity is known, models can estimate viscosity of emulsified oil as a function of the water content

$$\nu_{oil} = \nu_{ref} \exp\left(\frac{C_{emul1} Y}{1 - C_{emul2} Y}\right)$$

(Betancour et al, 2005)



The viscosity of non emulsified oil depends on temperature and evaporation

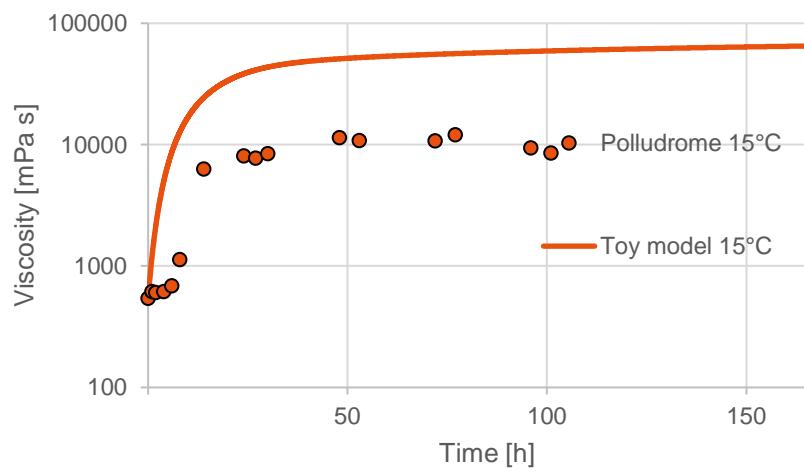


$$\nu_{oil} = \nu_{ref} \exp \left(C_{temp} \left(\frac{1}{T} - \frac{1}{T_{ref}} \right) + C_{evap} F_{evap} \right)$$

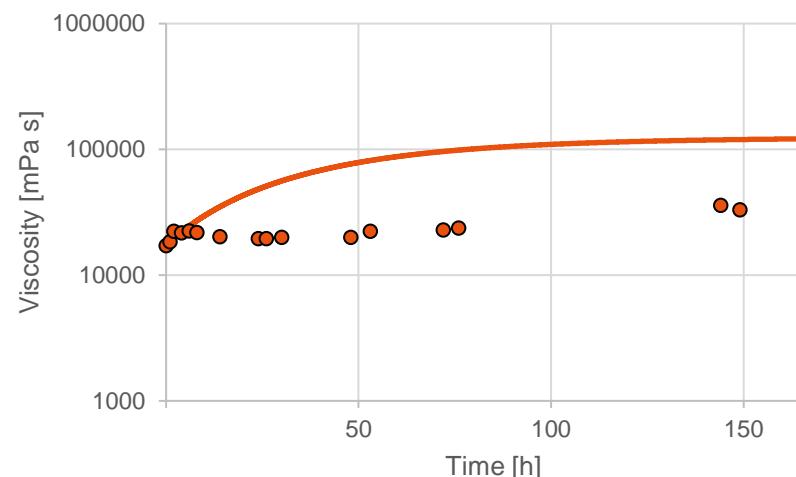
Model can make reasonable prediction of the evolution of slick viscosity

$$\nu_{oil} = \nu_{ref} \exp \left(C_{temp} \left(\frac{1}{T} - \frac{1}{T_{ref}} \right) + C_{evap} F_{evap} + \frac{C_{emul1} Y}{1 - C_{emul2} Y} \right)$$

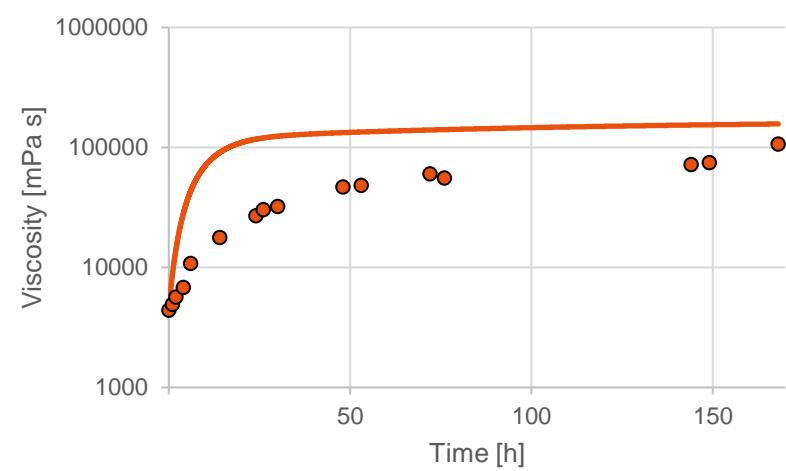
IM5



IM14



IM15



Take home message

Are the existing parameterizations able to simulate VLSFO weathering?

Yes, they can

Should you trust in oil weathering model forecast for VLSFO?

Only if an accurate oil characterization is available

Oil slick spreading should be improved to take into account the 'rheofluidity'

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Final conference

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